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煤层气井堵塞型递减原因分析及治理

——以延川南煤层气田为例

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摘要:延川南煤层气田部分井在生产过程中出现产气、产液异常快速递减的堵塞型生产特征。为了分析堵塞产生的原因,基于气井产液、水质、检泵等生产动态信息的变化,明确了堵塞主因包括结垢和煤粉两个方面,在分析结垢和煤粉堵塞形成机理的基础上开展了针对性预防和治理措施。针对结垢堵塞井形成常态化阻垢剂防垢与多级脉冲冲击波解堵相结合的防治措施,16口井增产效果较好,平均单井累计增产 $30.11\times 10^4\text{m}^3$ 。针对煤粉堵塞井形成自循环和空心杆洗井携煤粉工艺及氮气泡沫洗井解堵治理措施,洗井携煤粉工艺可有效缓解煤粉堵塞等导致的检泵,气井免修期延长60%;氮气泡沫解堵应用4口井均取得显著增产效果,平均单井增产 $1.25\times 10^4\text{m}^3/\text{d}$ 。成果认识为堵塞型煤层气井原因分析和治理对策提供了借鉴。

关键词:深煤层;煤粉;结垢;堵塞;解堵

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Cause analysis and treatment of coal-bed gas well plugging decline: A case study of southern Yanchuan CBM Field

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Abstract: In the production process, part of the wells in southern Yanchuan CBM Field has the plugging characteristics of abnormal and rapid decline of gas production and liquid production. In order to analyze the causes of blockage, based on the changes of the production dynamic information of the liquid recovery, water quality and pump check of wells, the main cause of plugging is clarified, including scaling and pulverized coal. On the basis of analyzing the formation mechanism of scaling and pulverized coal blockage, the targeted prevention and treatment measures are carried out. For the scaling plugging wells, form a treatment measure combining the normal prevention by adding scale inhibitor and the plugging removal by multi-stage pulse shock wave. 16 wells implemented by multi-stage pulse shock wave have got a good production increase with an average production increase of $30.11\times 10^4\text{m}^3$ per well. For the pulverized coal plugging wells, coal-carrying process by self-circulation and hollow rod well washing, and nitrogen foam well-unblocking treatment measures are formed. Well washing for carrying pulverized coal effectively alleviate the pump check caused by pulverized coal blocking pump, the gas well repair free period extended by 60%. Four wells applied the nitrogen foam for unblocking achieve significant production increase, with an average daily production increase of $1.25\times 10^4\text{m}^3$ per well. The results provide references for the cause analysis and treatment of blocked CBM wells.

Keywords: deep coal seam; pulverized coal; scale formation; plugging; plug removal

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为明确煤层气井低产的原因,国内研究者从地质、压裂、排采3个方面进行了研究,低产原因主要分为3个方面^[1-9]:①煤层埋藏浅或靠近断层、顶底板封盖性差等原因导致含气量低,是低产的主要地质原因;②针对高应力深煤层、构造煤等常规压裂改造工艺不匹配,压裂改造效果差,单井控制储量小导致产气量低;③排采过程中煤粉沉降,地层水结垢等堵塞渗流通道,导致产气量递减。针对非地质原因造成的递减,主要的增产措施有氮气泡沫压裂、活性水重复压裂、酸化解堵、震荡解堵等^[10-13]。对于深层煤层气井而言,煤层埋深大、地应力高、孔隙度及渗透性差,排采过程中渗流通道更容易被堵塞。延川南气田气井检泵过程中存在管杆结垢严重、泵筒煤粉聚集等现象,结垢和煤粉沉降发生在近井地层堵塞渗流通道。气田部分井在生产过程中表现出产液量和产气量异常递减,反应出典型的堵塞型生产特征。如何准确识别气井结垢和煤粉形成的主要原因及规律变化,构建针对结垢和煤粉问题的一体化防治对策,降低地层堵塞风险和井筒异常频次,保持渗流通道畅通和气井正常生产时率,对实现深层煤层气稳产具有重要意义。

1 气田基本情况

延川南煤层气田位于鄂尔多斯盆地东南缘,构造上处于渭北隆起和晋西挠褶带交汇处,整体为西倾单斜构造,中部北东向的西掌断裂带将气田分为东西两部分,东部为谭坪构造带,西部为万宝山构造带,区内发育小断层,煤储层非均质性强。煤层气开发主力煤层为下二叠统山西组2号煤层,东部谭坪构造带2号煤层埋深较浅,埋深介于600~1 000 m,平均为880 m,向西埋深逐渐增加,万宝山构造带2号煤层埋深介于1 000~1 500 m,平均为1 300 m。含气量随埋深增加逐渐增大,平均为11.3 m³/t。2号煤层全区横向分布稳定且连续,煤层平均厚度约为5 m,平面上煤层厚度呈东南厚,向北部及西部减薄的趋势,在谭坪构造带煤厚介于5.0~5.5 m,万宝山构造带煤厚介于4.5~5 m,煤层一般含1~2层夹矸,局部地区发育3层夹矸,夹矸总厚介于0~0.80 m,平均为0.35 m,由西向东夹矸厚度增加,层数增多。镜质体反射率 R_o 介于1.96%~3.22%,平均为2.45%,整体处于贫煤、无烟煤阶段,随埋深的增加变质程

度增大,平面上由东向西 R_o 逐渐增大。镜质组含量介于76.1%~89.2%,平均为83.0%,煤的生、储气物质基础较好。煤体结构以原生结构煤和块状碎裂煤为主,气田北部和南部边缘局部发育碎粒煤和糜棱煤,煤层渗透率介于 $(0.2\sim 0.5)\times 10^{-3}\mu\text{m}^2$,平均为 $0.344\times 10^{-3}\mu\text{m}^2$,孔隙度介于3.0%~6.7%,属特低孔低渗储层。煤储层压力在东部谭坪构造带介于2.77~4.79 MPa,平均为3.91 MPa,在西部万宝山构造带介于4.47~10.57 MPa,平均为7.98 MPa。水动力条件分区特征明显,谭坪构造带及万宝山构造带东北部为弱径流区,地层水矿化度介于3 000~5 000 mg/L,水型为NaHCO₃,万宝山构造带中西部以高压封闭滞留区为主,地层水矿化度介于10 000~160 000 mg/L,以CaCl₂水型为主(图1)。

2 排采水变化规律

煤层气产出机理是排水降压、解吸产气,排采过程主要分为排水期、上产期、稳产及递减期3个阶段。产液量以及水质随着生产时间的延长呈现规律性的变化。排水期产液20~100 m³/d,上产期产液10~20 m³/d,高产稳产期产液0.5~5.0 m³/d。排采水矿化度在平面上西高东低,西部万宝山构造带稳定矿化度在10 000~160 000 mg/L,一般是投产初期矿化度的2倍,水型自始至终为CaCl₂。

位于万宝山构造带西南部高矿化度区的某平台4口井的产液及水质变化曲线如图2、图3所示,早期排水期为单向水流阶段,产液量最高,产出液以压裂液与地层水混合液为主,矿化度较低。进入解吸上产期后,随着解吸气量增加,气相相对渗透率增大,产液量逐步降低,产出液中地层水占比增加,矿化度逐步增高。在稳产及递减期,渗流通道以气相渗流为主,产液量低且以高矿化度的地层水为主。产液量和水质的变化带来了两方面的问题:一是高矿化度地层水产出后,煤层气大量解吸引起的储层温度、压力变化,井筒内流速改变,诱导地层水结垢;二是产液量降低后携煤粉能力减弱,煤粉在井筒、泵筒和近井地带堆积。以上两方面问题既导致机抽排液不正常,又导致近井地带的渗流通道堵塞。因此,煤层气井排采水动态变化导致气井结垢和煤粉堵塞成为气田开发必然要面对的问题。

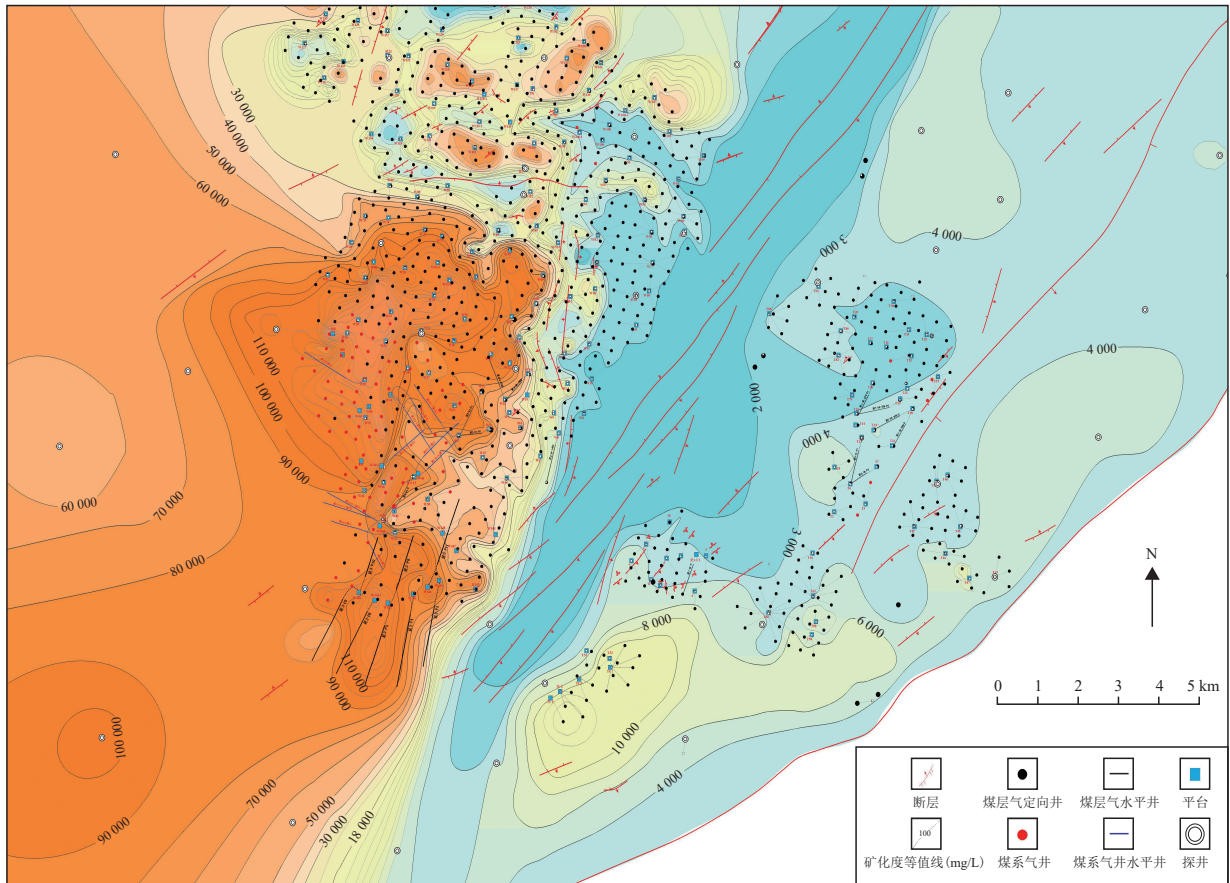


图1 延川南煤层气田地层水矿化度等值线

Fig. 1 Water salinity isoline of southern Yanchuan CBM Field

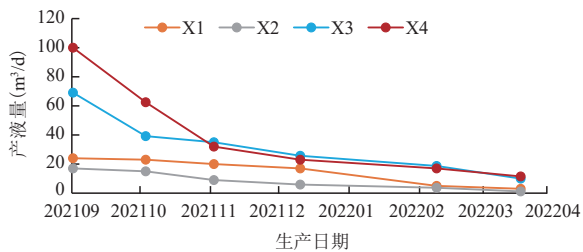


图2 产液量变化曲线

Fig. 2 Variation curve of liquid production

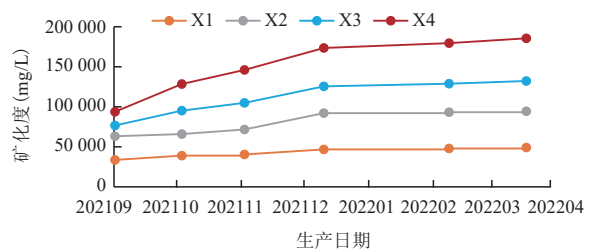


图3 矿化度变化曲线

Fig. 3 Salinity change curve

3 煤粉产出运移分析及其影响

3.1 煤粉的来源及运移条件

煤层中煤粉来源包括构造变形产生的原生煤粉和钻井、压裂、排采过程中的机械破坏以及应力改变产生的次生煤粉,其中构造变形产生的原生煤粉是

主要来源。煤粉运移包括两方面:一是煤层内的径向运移,二是井筒中垂直运移。影响煤粉正常运移的情况一般分为两种:一是在排采过程中由于流体流动、压力激动等造成煤粉运移,调整冲次或异常停抽时流速改变煤粉沉降堵塞渗流通道;二是煤层气井排采后期产液量变低,低液量难以将煤粉有效携带出井筒,逐步在井筒和近井地带堵塞产气通道^[14-15]。

3.2 煤粉对产量的影响

煤粉对产量影响分为两方面,一是地层中煤粉运移沉降,堵塞孔隙喉道或者侵入压裂支撑缝(图4),降低储层渗透率和裂缝导流能力,导致产气和产液量的同时下降;二是在排采中后期产液量极低的情况下,地层产出的煤粉难以携带出井筒,慢慢在井筒聚集,造成卡泵、埋泵等影响正常举升排液,进而影响气井生产时率^[16-18]。通过统计近3年的检泵(图5)发现,因煤粉造成的泵堵、卡泵等原因导致的修井作业约占50%,特别是部分井由于出煤粉严重导致频繁检泵,严重影响了气井的正常生产。

4 成垢因素分析及其影响

4.1 井筒成垢原因分析

为研究煤层气井结垢原因,对垢的成分进行了

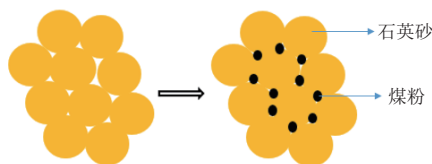


图4 煤粉堵塞示意图

Fig. 4 Schematic diagram of pulverized coal plugging



图5 油管被沉降的煤粉堵塞

Fig. 5 Oil pipe blocked by settling pulverized coal

分析,通过X射线衍射光谱仪对样品所含化合物监测表明,垢的主要成分为碳酸钙和少量铁的化合物;采用X射线荧光光谱仪对垢样所含元素的质量分数进行测定(表1),占质量分数最高的为Ca元素。同时对排采水中的离子进行分析(表2),排采水中阳离子主要有 Na^+ 、 K^+ 、 Mg^{2+} 、 Ca^{2+} ,阴离子主要有 Cl^- 、 SO_4^{2-} 、 HCO_3^- ,阳离子中除 Na^+ 外, Ca^{2+} 质量浓度远高于其他阳离子质量浓度,阴离子中 HCO_3^- 质量浓度也较高。结垢的主要化学反应: $\text{Ca}^{2+}+2\text{HCO}_3^- \rightarrow \text{Ca}(\text{HCO}_3)_2$,
 $\text{Ca}(\text{HCO}_3)_2 \rightarrow \text{CaCO}_3 \downarrow + \text{CO}_2 \uparrow + \text{H}_2\text{O}$ 。在热力学条件没有发生变化、平衡状态没有被打破的时候,会持续一种稳定的状态,此种情况下不会产生结垢;在煤层气井排水降压过程中,近井地带地层及井筒温度、压力、流体流态发生变化,打破了原有的平衡,随着流压及储层压力的不断降低。当水中 CO_2 分压低于 CaCO_3 溶解平衡所需要压力时,反应平衡会向右进行,形成 CaCO_3 结垢。

4.2 结垢对产量的影响

结垢对产量的影响也表现在两个方面:一是近

表1 垢样元素质量分数

Table 1 Mass fraction of scale elements

元素组分	质量分数(%)
Ca	76.393
Fe	17.164
Mg	0.332
Al	0.124
Si	0.342
P	0.008
S	2.344
Na	0.417
Mn	0.412
Cu	0.300
Zn	0.008
Sr	1.365
Ba	0.305

表2 排采水离子构成(质量浓度)

Table 2 Ion composition of production water(mass concentration)

Na^+	K^+	Mg^{2+}	Ca^{2+}	Cl^-	SO_4^{2-}	CO_3^{2-}	HCO_3^-	mg/L
16 000.65	112.87	1 858.22	7 580.83	46 750.00	1 039.07	0	533.93	

井筒地层或射孔炮眼结垢造成渗流通道堵塞,影响地层流体产出;二是管杆泵结垢后容易导致卡泵、遇阻等异常工况,影响气井正常排液生产。

5 地质与工艺一体化治理对策

5.1 煤粉治理

理论上,在连续排采的条件下,产水量大于携带煤粉的临界流量,煤粉就能随水排出,如果产水量小于携带煤粉的临界流量,煤粉就会不断堆积。针对煤粉在泵筒堆积导致的泵堵问题,以提高液体流速从而提升携煤粉能力为治理方向,形成了自循环洗井和空心杆洗井两种工艺。自循环洗井是通过隔膜泵向油套环空持续补水,保证注入水量与管式泵排水量基本相当,既增加携带煤粉的流速,又避免补水对产气的影响,该工艺对中低产井较为适用,应用150口井,免修期提升60%。对于瞬时产气量大于 $300\text{ m}^3/\text{h}$ 的高产井,通过环空注入的水容易被产气携带至气流程,因此,针对高产气井采用空心杆洗井工艺(图6),通过空心抽油杆注水至活塞上部,与通过泵筒进入油管的地层水混合,增加液体在油管内的流速,从而提升煤粉携带能力。该工艺已应用5口井,混合产出液初期含大量煤粉,气井免修期有效延长。

针对煤粉在近井地带沉降堵塞渗流通道的问题探索开展了氮气泡沫洗井,煤层气生产后期地层能量低,常规清水洗井漏失量大难以建立循环,氮气泡沫体系低密度、低滤失特征可以建立循环,同时泡沫体系的高膨胀能冲击堵塞通道的煤粉,并具有强悬浮能力将煤粉携带出来,从而疏通井筒及近井地层堵塞。累计在4口水平井开展现场试验,均取得较好增产效果,平均单井增产 $1.25\times 10^4\text{ m}^3/\text{d}$ 。典型井生产曲线如图7所示,洗井前产气异常递减,2个月内

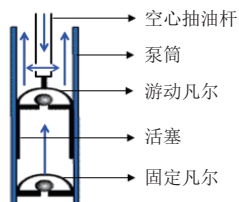


图6 空心抽油杆洗井原理

Fig. 6 Principle for well washing by hollow sucker rod

产量由 $2.0\times 10^4\text{ m}^3/\text{d}$ 递减至 $0.6\times 10^4\text{ m}^3/\text{d}$,洗井过程中返出煤粉及少量压裂砂(图8),洗井后产量恢复至前期高产稳产水平。

5.2 结垢治理

针对井筒结垢的治理,包括预防性对策和进攻性对策,预防性对策主要通过阻垢剂的络和增溶作用、静电斥力作用等,防止或减缓管杆的结垢。针对已经结垢造成的近井堵塞,目前进攻性的解堵措施主要有酸洗和振动解堵两类,考虑酸洗解堵对套管及管杆腐蚀性大,以及返排液处理难度大等因素,气田主要开展了多级脉冲冲击波增透解堵措施。通过脉冲功率技术将高功率电磁能量转换为机械能作用于储层,产生冲击、剪切作用,破碎堵塞的垢片,同时,在近井筒破裂煤层形成裂缝,解除近井堵塞^[19-20]。目前气田实施冲击波增透解堵37井次,措施有效率为88%,平均措施有效天数为594 d,增产效果较好井16口,平均单井累计增产 $30.11\times 10^4\text{ m}^3$ 。

6 结论

1) 煤层气井排采过程中产液量逐步减小、矿化度逐步升高的变化规律是结垢和煤粉聚集的诱导因素,由此导致的堵塞递减是煤层气井生产过程中普遍面临的问题。

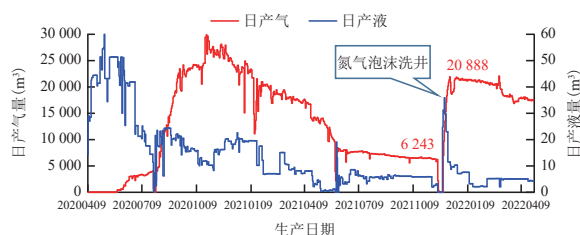


图7 氮气泡沫解堵井生产曲线

Fig. 7 Production curve of nitrogen foam plug removal wells

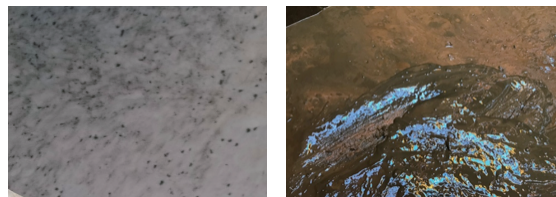


图8 氮气泡沫洗井返出煤粉

Fig. 8 Pulverized coal carried out by nitrogen foam

2) 延川南气田气井结垢的主要成分为 CaCO_3 , 通过优选阻垢剂具有较好的预防效果,多级脉冲冲击波通过物理致裂对已经结垢堵塞的井具有较好解堵效果。解堵后的井需要配套预防性防垢措施,延长解堵的有效期。

3) 煤层气井生产后期产液量普遍低于携带煤粉的临界流速,通过自循环洗井和空心杆洗井增大管柱液体流速可以有效减少煤粉沉降聚集,延长气井免修期。氮气泡沫洗井可以有效疏通近井筒煤粉堵塞,对因煤粉堵塞造成的异常递减井具有显著增产效果。

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